

# SLIP COMPLEXITY AND FRICTIONAL HETEROGENEITIES IN DYNAMIC FAULT MODELS

S51F-02

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- Earthquakes are complex at all scales, both in slip on the fault surface and in the stress drop;
- First evidences in Das and Aki (1977a), Aki (1979), Day (1982);
- First attempts to model complexities were the "asperity " model of Kanamori and Stewart (1976) and the " barrier " model of Das and Aki (1977b);
- Madariaga (1979) showed that the seismic radiation from these models would be very complex;
- Bak et al. (1987) suggested that complexity must be due to the spontaneous organization of a fault that is close to criticality.



#### The slip complexity on a fault may arise from:

- Numerical artefacts and spurious pollutions of the solutions due to violation of stability and convergency conditions or grid dispersion;
- Effects of heterogeneous distribution of initial stress;
- Inhomogeneities in the mechanical and rheological properties of the fault ( expressed in terms of heterogeneity of frictional parameters );
- Modifications of governing equation;
- Coupling of two modes of propagation in a *truly* 3 D earthquake model;
- Interactions with other active faults;
- Geometrical complexity, non planarity, fault segmentation and branching;
- Different and competing physical mechanisms occurring within the cosesimic temporal scale, like thermal pressurization, rock melting, mechanical lubrication, ductile compaction of gouge, etc..

# Statement of the problem and methodology

We solve *fully* dynamic, spontaneous problem ( the fundamental elasto–dynamic equation ), without body forces **f** 

$$\rho \ddot{U}_i = \sigma_{ij,j} + f_i$$

We consider 2–D pure in–plane (or mode II) problem, for which solutions (for instance the fault slip, i. e. the particle displacement discontinuity) are in the form:  $\mathbf{u} = (u_1(x_1, t), 0, 0) \dots$ 







The spatial computational domain is discretized using equilateral triangles in 2–D problems and cubic building blocks in 3–D one. The medium is linearly elastic except that in the fault plane ...

... that obeys to the Fault Boundary Condition, i. e. to the governing law, that relates the fault friction  $\tau$  to some physical observables. In general is:

 $\tau = \mu(u, v, \Psi, T, H, \lambda_c, h, g, C_e) \sigma_n^{eff}(\sigma_n, p_{fluid})$ 

where  $\mu$  is the friction coefficient and  $\sigma_n^{eff}$  the effective normal stress.

Slin wookoning low ( Paranhlatt		$\begin{bmatrix} & (v_1) & (\psi_1) \end{bmatrix}$
$\tau = \left\{ \left[ \mu_u - (\mu_u - \mu_f) \frac{u}{d_0} \right] \sigma_n^{eff} \right\}$	$, u < d_0$	$\int \tau = \left[ \mu_* - a \ln \left( \frac{\sigma_*}{v} \right) + b \ln \left( \frac{T \sigma_*}{L} \right) \right] \sigma_n^{eff}$
$\begin{bmatrix} \mu_f \sigma_n^{eff} \end{bmatrix}$	, $u ≥ d_0$	$\left \frac{\mathrm{d}}{\mathrm{d}t}\Psi = 1 - \frac{\Psi v}{L} - \left(\frac{\alpha_{LD}\Psi}{b\sigma_n^{eff}}\right)\frac{\mathrm{d}}{\mathrm{d}t}\sigma_n^{eff}\right $

An explicit displacement discontinuity is assumed between the two sides of the fault: **Traction–at–Split–Nodes** scheme (Day, 1982a, 1982b; <u>Andrews, 1999</u>)

The numerical details and the implementations of constitutive equations is given in Bizzarri et al. (2001, GJI, 144, 656-678) and in Bizzarri and Cocco (2005a, Ann. Geophys, 48, 2, 279-299)

#### Dynamic rupture propagation



Bizzarri and Cocco ( 2003, JGR, 108, B8, 2373 )











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#### Implications for fracture energy



In the location  $\mathbf{x}$  on the fault plane we estimate the "Fracture Energy " accordingly to the formula ( e. g. Ida, 1972 ):

$$E_{G}(\mathbf{x}) = \frac{1}{2} \int_{0}^{d_{0}^{eq}} \left( \tau(\mathbf{x}, t) - \tau_{f}^{eq}(\mathbf{x}) \right) \mathrm{d} u$$

#### but

#### Is Fracture Energy Surface Energy ?

Remember **POSTER S41B–0997** by Pittarello, Di Toro, Bizzarri, Pennacchioni, Hadizadeh







#### The rake variation #1



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#### Fault slip time snapshots – Linear SW assumed



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1 – D Fourier's heat conduction equation:

 $\frac{\partial}{\partial t}T = \chi \frac{\partial^2}{\partial \zeta^2}T + \frac{1}{c}q$ 

Coupling of temperature T with pore fluid pressure  $p_{fluid}$ :

$$\frac{\partial}{\partial t} p_{fluid} = \frac{\alpha_{fluid}}{\beta_{fluid}} \frac{\partial}{\partial t} T - \frac{1}{\beta_{fluid}} \frac{\partial}{\partial t} \Phi + \omega \frac{\partial^2}{\partial \zeta^2} p_{fluid}$$

where  $\chi$  is the thermal diffusivity, *c* the heat capacity for unit volume,  $\alpha_{fluid}$  the coefficient of thermal expansion,  $\beta_{fluid}$ the compressibility coefficient,  $\Phi$  the porosity and  $\omega = k/\eta_{fluid}\beta_{fluid}\Phi$  the hydraulic diffusivity (being *k* the permeability of the medium and  $\eta_{fluid}$  the dynamic fluid viscosity). Analytical solutions at  $\zeta = 0$  are:

$$T^{w^{f}}(\xi_{1},\xi_{3},t) = T_{0}^{f} + \frac{1}{2 cw(\xi_{1},\xi_{3})} \int_{0}^{t-\varepsilon} dt' \operatorname{erf}\left(\frac{w(\xi_{1},\xi_{3})}{2\sqrt{\chi(t-t')}}\right) \tau(\xi_{1},\xi_{3},t') v(\xi_{1},\xi_{3},t')$$

$$\begin{split} \widetilde{p}_{fluid}^{w^{f}}\left(\xi_{1},\xi_{3},t\right) &= p_{fluid_{0}}^{f} + \frac{\gamma}{2w(\xi_{1},\xi_{3})} \int_{0}^{t-\varepsilon} \mathrm{d}\,t' \left\{-\frac{\chi}{\omega-\chi} \operatorname{erf}\left(\frac{w(\xi_{1},\xi_{3})}{2\sqrt{\chi(t-t')}}\right) + \frac{\omega}{\omega-\chi} \operatorname{erf}\left(\frac{w(\xi_{1},\xi_{3})}{2\sqrt{\omega(t-t')}}\right) \right\} \\ &\left\{ \tau\left(\xi_{1},\xi_{3},t'\right) v\left(\xi_{1},\xi_{3},t'\right) - \frac{2w(\xi_{1},\xi_{3})}{\gamma} \frac{1}{\beta_{fluid}} \Phi(t') \frac{\partial}{\partial\,t'} \Phi(\xi_{1},0,\xi_{3},t') \right\} \end{split}$$

Bizzarri and Cocco ( 2005c, 2005d, *JGR*, submitted June 2005 )







 Spatial heterogeneities in the constitutive parameters make us able to simulate different behaviors, like barrier – healing and self – healing pulses;

 The regularization of the governing laws is an alternative to have self – healing;

 Slip complexity may arise considering a heterogeneous initial stress and rake rotation during the rupture propagation;

The inclusion of the so – called second – order physical effects, like thermal pressurization of pore fluid, changes the traction evolution within the cohesive zone and the rupture shape.

# Thank you!

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#### Remembering the dimensionality of the problem:

- 2 D Mode II ( pure in plane ):  $u = (u_1(x_1,t), 0, 0)$
- 2 D Mode III ( pure anti plane ):  $u = (0, u_2(x_1, t), 0)$
- 3 D Mixed mode:  $u = (u_1(x_1,t), u_2(x_1,t), 0)$
- 3 D having only one non null component:  $\mathbf{u} = (u_1(x_1, x_2, t), 0, 0)$
- **Truly** 3 D:  $\mathbf{u} = (u_1(x_1, x_2, t), u_2(x_1, x_2, t), 0)$

#### DIETERICH IN REDUCED FORM WITH HEALING

$$\begin{cases} \tau = \left[ \mu_* - \alpha \ln \left( \frac{v_*}{v} + 1 \right) + b \ln \left( \frac{\Psi v_*}{L} + 1 \right) \right] \sigma_n^{eff} \\ \frac{d}{dt} \Psi = \frac{\gamma_{fh} - \Psi}{L} - \frac{\Psi v}{L} \end{cases}$$

 $\gamma_{fh} = 1 \text{ s}$ 

 $t_{fh}$  is the time for healing (slip duration)

Evolution law proposed by <u>Nielsen et</u> <u>al. (2000)</u> and by Nielsen and Carlson (2000). Used in this form by Cocco et al. (2004)

#### DIETERICH IN REDUCED FORM REGULARIZED

$$\tau = \left[ \begin{array}{c} \mu_{*} - a \ln \left( \frac{v + v_{*}}{v + v_{*}} \right) + b \ln \left( \frac{\Psi(v - v)}{L} + 1 \right) \right] \sigma_{n}^{eff}$$
$$\frac{d}{dt} \Psi = 1 - \frac{\Psi(v + v_{*})}{L}$$

 $v_r$  is a regularization fault slip velocity

<u>Perrin et al. (1995)</u>, Cocco et al. (2004)

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Bizzarri and Cocco (2005a, Ann. Geophys., 48, 2, 279-299)



Initial stress is based on the Hartzell and Heaton (1983) Imperial Valley Earthquake model:

http://www.seismo.ethz.ch/srcmod/Eventpages/s19791 MPERIhart.html

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