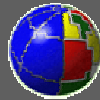


*Università degli Studi di Bologna
Dottorato di Ricerca in Geofisica – XXI Ciclo*

MODELLI DINAMICI DI ROTTURA SISMICA

Dr. Andrea Bizzarri, Ph.D.

Istituto Nazionale di Geofisica e Vulcanologia
Sezione di Bologna



September 2006

Index

1. EARTHQUAKE SOURCE DYNAMICS

- Elasto – dynamic problem
- Rupture description
- Dislocation vs. crack models
- Forward modeling scheme
- Rupture stages

2. FAULT GOVERNING LAWS (CONSTITUTIVE EQUATIONS)

- Fault models
- Physical phenomena in faulting
- Fracture criteria and constitutive laws
- Strength and constitutive laws
- Slip – dependend friction laws
- Rate – and state – dependent friction laws

3. EARTHQUAKE NUCLEATION

4. 1 – D SPRING – SLIDER MODEL

- Numerical method
- Fault seismic cycle modeling
- Analytical stress perturbations
- Rhealistic stress perturbations

5. RUPTURE PROPAGATION IN 2 – D FAULT MODELS

- Numerical methods
- BIE vs. FD
- Slip – weakening vs. Dieterich – Ruina law
- The cohesive zone and the breakdown processes
- Theoretical interpretations and correspondency formula
- The estimate of d_0 and related problems
- The importance of the evolution equation

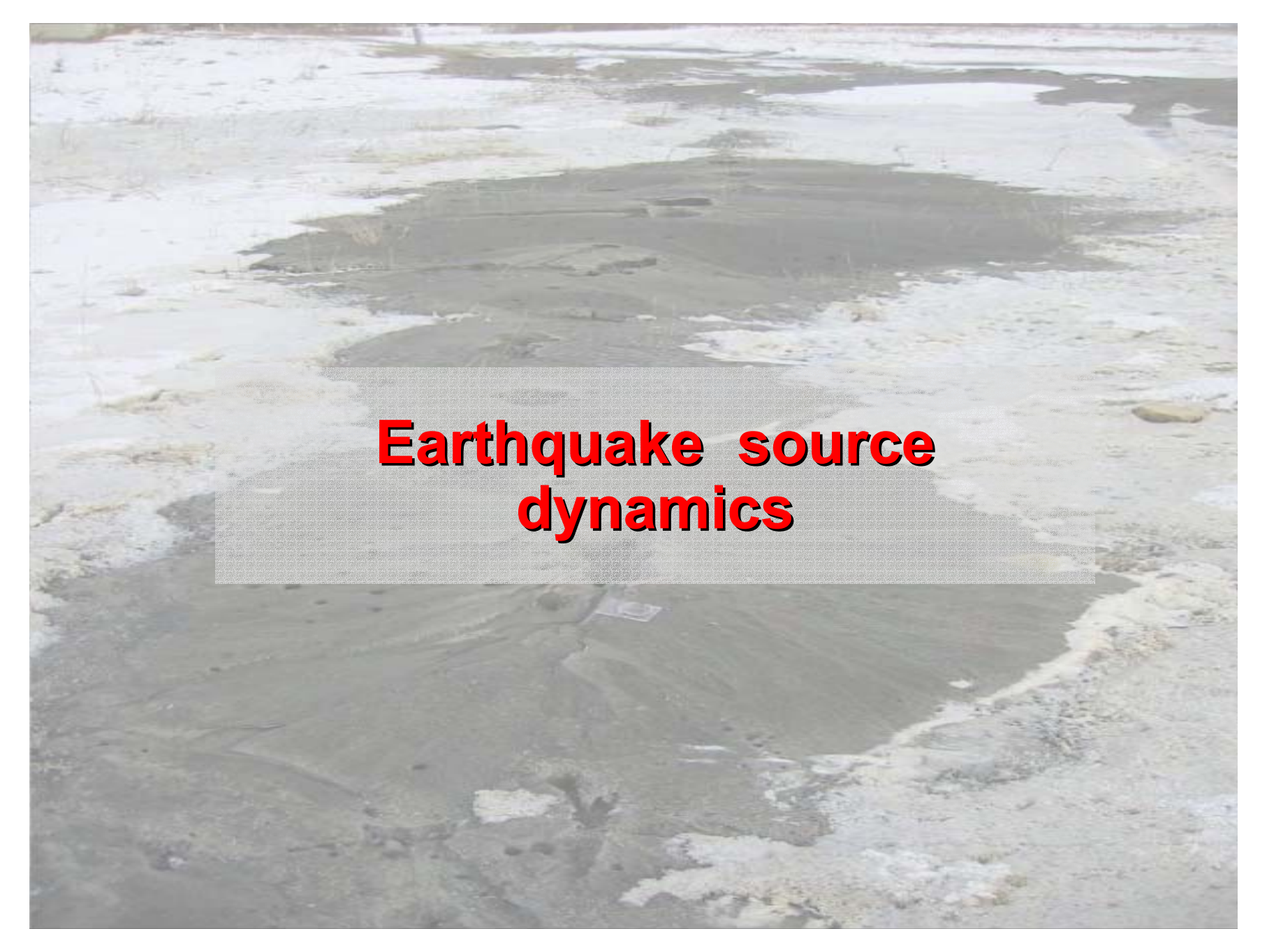
6. RUPTURE PROPAGATION IN A TRULY 3 – D FAULT MODEL

- The numerical method
- The reference case. Comparison between 2 – D and 3 – D models
- Coupling of two modes of propagation. The rake variation
- Dependence on the absolute stress level. Symmetry leak
- Heterogeneous configurations

7. RHEOLOGICAL HETEROGENEITIES, CRACK ARREST AND HEALING PHENOMENA

- The crack and arrest models
 - The barrier – healing
 - The pseudo self – healing
- The pulse
 - Different materials
 - Analytical modifications to friction laws
 - The Nielsen's model

8. CONVERGENCE

An aerial photograph of a coastal or estuarine area. The central part of the image is dominated by a large, dark, irregularly shaped area that appears to be water or a thick layer of mud. This dark area is surrounded by lighter-colored, sandy or silty ground. There are some small, scattered patches of vegetation and what looks like a small structure or marker in the lower-left quadrant of the dark area. The overall scene suggests a natural or possibly human-altered coastal environment.

**Earthquake source
dynamics**

Elasto - dynamic problem

- * **Solution of the fundamental elasto – dynamic equation (i. e. the II law of dynamic for continuum media):**

$$\rho(d^2/dt^2)U_i = \sigma_{ij,j} + f_i \quad ; i = 1, 2, 3$$

where:

ρ is the mass cubic density,

\mathbf{U} is the particle displacement vector ($\mathbf{U} = \mathbf{x}' - \mathbf{x}$),

$\{\sigma_{ij}\}$ is the stress tensor; $\sigma_{ij} = C_{ijkl}e_{kl}$; $i,j,k,l = 1, 2, 3$, where C_{ijkl} is the elastic constant tensor, accounting for the rheology of the medium and e_{kl} is the strain tensor ($e_{kl} = 1/2 (U_{k,l} + U_{l,k})$),

\mathbf{f} is the body force vector.

* *Choice of the dimensionality d of the problem
($1 - D, 2 - D, 3 - D$).
($d = \text{rank of the } \mathbf{U} \text{ array, i. e. number of equations}$)*

1. Wave propagation problem: Hyperbolic PDE
 D' Alembert wave equation:

$$\nabla^2 \mathbf{U} - (1/c_0) (\partial^2 / \partial t^2) \mathbf{U} = 0$$

where c_0 is the wave speed.

2. Rupture problem



Rupture Description

Following *Scholz (1990)* the rupture can be described by using:

- * ***CRACK MODELS:***

The energy dissipation at crack edge (or crack tip) is paramount. Describe explicitly the crack propagation.

- * ***FRICTION MODELS:***

The effects at the edges are not explicitly considered. Explicitly allow for the calculation of the evolution of stress tensor components in terms of material properties of the fault.

Dislocation vs. Crack Models

DISLOCATION MODELS

- * Study of **displacement discontinuity**
- * **Slip** is assumed to be constant on the fault;
The fault evolution is represented by unilateral or bilateral motion (rectangular dislocations: Haskell' s model)
- * **Kinematic description** it accounts for time evolution of rupture front and it neglects dynamics of faulting

↑ Long period seismic waves modeling ($\lambda \geq L_{fault}$)

↓ constant dislocation is inadmissible;
strain energy at crack tip is unbounded;
stress drop is infinite

CRACK MODELS

- * Impose **finite energy flow** into the rupture
 - * **Slip is not prescribed**,
but it is calculated from the stress drop and from the fault strength S^{fault}
 - * **Dynamic description**: the shear stress drops inside the crack (after nucleation processes), increases the stress outside the crack (near the crack tip) and tends to facilitate further grow of the rupture
- ↑ The motion is determined by fracture criterion (and eventually by the assumed constitutive law on the fault)
- ↑ The problem is characterized by assuming the boundary conditions on the fault plane. It has mixed b. c.: slip assigned outside the crack tip and stress tensor components inside the crack tip

Forward modeling scheme

1. *Fault model:*

- **Fault geometry** (orientation, planar or non – planar, ...)
- **Fault system** (multiple segments, multiple faults, ...)



2. *Medium surrounding the fault surface(s)*

- **Properties of the medium** surrounding the fault(s): cubic mass density structure, velocity structure, anisotropy, attenuation

3. *Choice of the dimensionality d' of the problem (1 – D, 2 – D, 3 – D, 4 – D).*

(d' = number of the independent variables in the solutions)



4. *Choice of the representation*



5. *Choice of the numerical method*

- (FE, FD, BE, BIE, SE, hybrid)

6. *Specification of the Boundary Conditions*

- **Domain** Boundaries Conditions (DBCs)
- **Fault** Boundary Condition (FBCs)
- **Auxiliary** Conditions (ACs)



7. *Specification of the Initial Conditions*

- Initial conditions **on the fault**: (initial slip, slip velocity, state variable, pre – stress);
- Initial conditions **outside the fault**: (tectonic load, (state of neighbouring faults: the fault is not an isolated system))

8. *Evaluation of the solutions*

- Convergence analysis (**consistency + stability**)

Rupture stages

1. Nucleation (quasi – static to dynamic evolution)

- *How can we simulate nucleation?*
- *How can we promote fault instability?*

2. Propagation

- *What is the fault constitutive equation (governing law)?*

3. Healing

- *What type of healing occurs?*
- *What controls fault healing?*

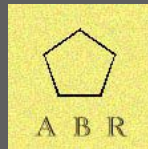
4. Rupture arrest

- *What is responsible of rupture arrest?*
- *How can we represent it? Earthquake energy balance?*

5. Fault re – strengthening

- *How can we model further instabilities episodes on the fault?*

This slide is empty intentionally.



Support Slides: Parameters, Notes, etc.

To not be displayed directly. Referenced above.

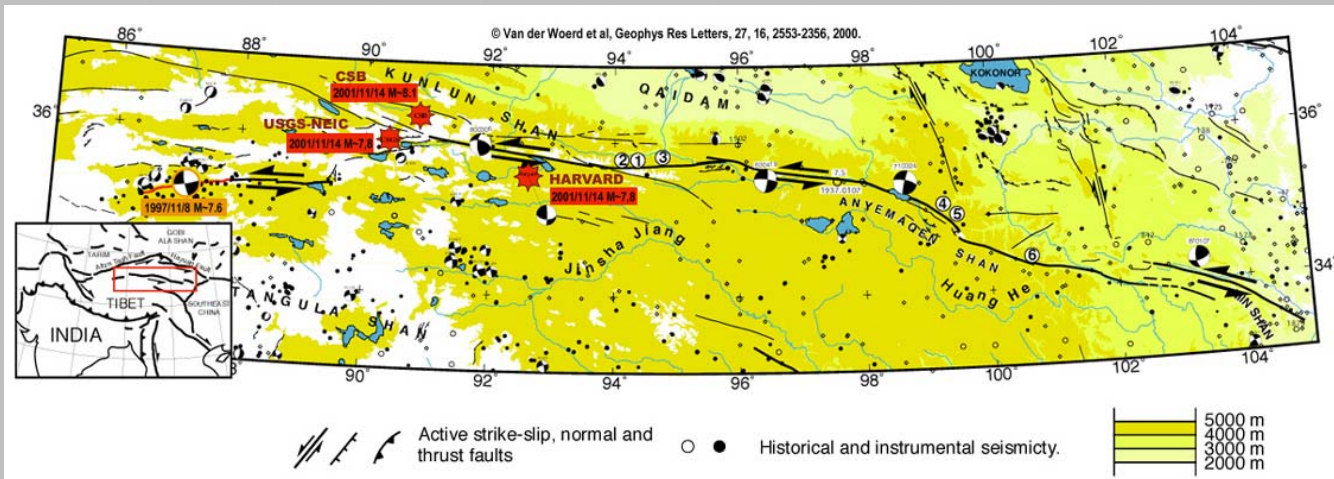
Geometrical complexity



Kokoxili
 M_w 7.9
earthquake
(Qinghai
Province,
China)

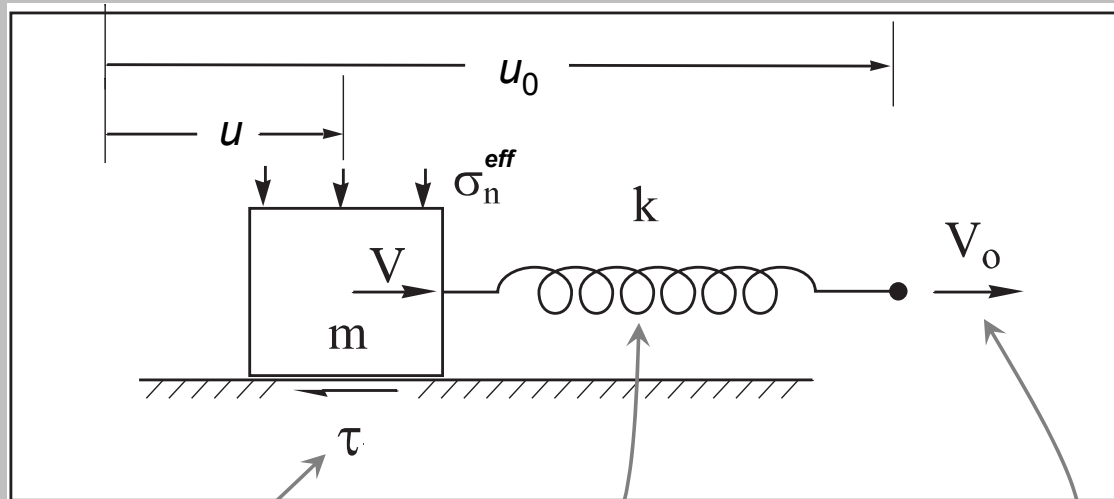


Strike Slip Surface Breaks



Dimensionality d'

1 – D Spring – Slider (mass – spring) model



Frictional sliding
(\leftrightarrow rheological properties)

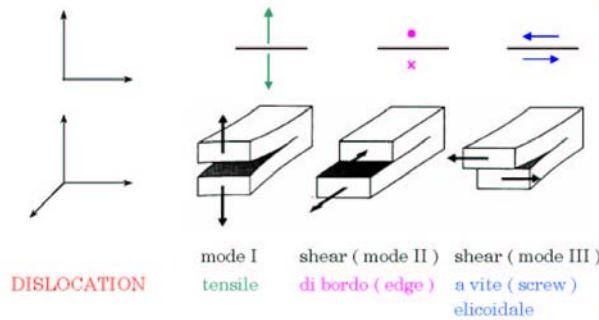
Elastic behaviour
(\leftrightarrow surrounding medium)

Loading velocity
(\leftrightarrow tectonic load)

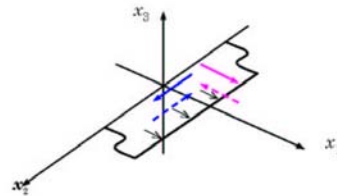
Fracture propagation modes

Elasotdynamics Fondam. Eq.: $\rho \ddot{u}_i = f_i + \sigma_{ij,j}$

Solution: $\mathbf{u}(\mathbf{x}, t)$ (mixture of shear crack and opening crack)



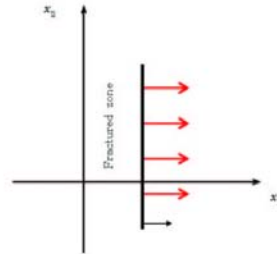
- opening cracks (mode I) $\mathbf{u} = (0, 0, u_3(\mathbf{x}, t))$ 4 - D
- shear cracks $\mathbf{u} = (u_1(\mathbf{x}, t), u_2(\mathbf{x}, t), 0)$ 4 - D
 - Planar fault surface ($x_3 = 0$) \Rightarrow on - fault coordinates: x_1, x_2
 - $\mathbf{u} = (u_1(x_1, x_2, t), u_2(x_1, x_2, t), 0)$ truly 3 - D
 - Propagation direction: x_1



- mixed mode $\mathbf{u} = (u_1(x_1, t), u_2(x_1, t), 0)$ pseudo 3 - D
- mode II (in - plane) $\mathbf{u} = (u_1(x_1, t), 0, 0)$ 2 - D
- mode III (anti - plane) $\mathbf{u} = (0, u_2(x_1, t), 0)$ 2 - D

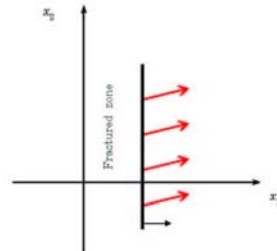
Shear rupture on a planar fault surface ($x_3 = 0$)
Snapshots at fixed time t

PURE MODE II



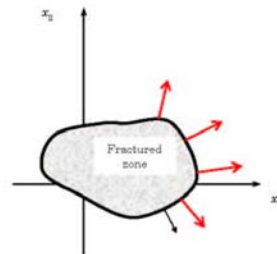
Dependence on x_1
Independence on x_2
 $\Rightarrow u_1(x_1, t)$

MIXED MODE



Dependence on x_1
Independence on x_2
 $\Rightarrow u_1(x_1, t)$
 $u_2(x_1, t)$

TRULY 3 - D



Dependence on x_1
 Dependence on x_2
 $\Rightarrow u_1(x_1, x_2, t)$
 $u_2(x_1, x_2, t)$

— Crack tip
 → Local crack enlargement direction

→ Local displacement

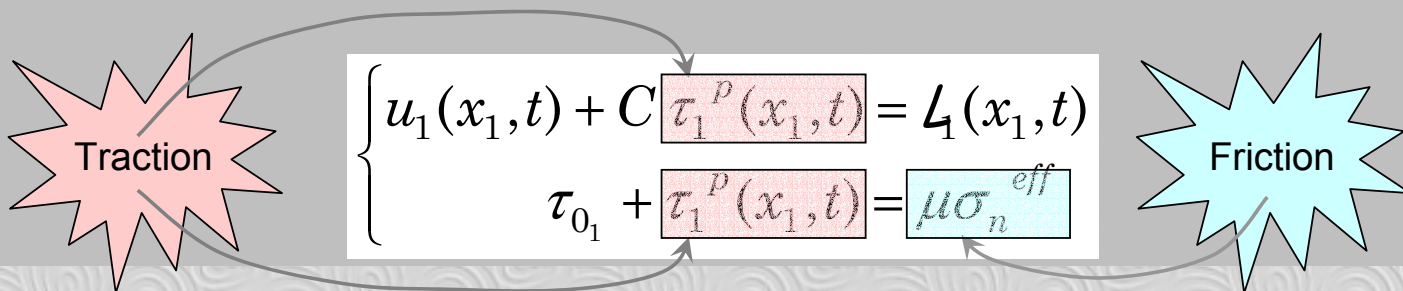
Representation

1. INTEGRAL REPRESENTATION

Source integral representation (*Betti*' s theorem, Integration in time (*Green – Volterra*' s relation), limit in fault surface, Lamb' s problem):

$$u_n(\mathbf{x}, t) = \int_{-\infty}^{+\infty} dt' \int_{S(t')} d\xi G_{n\alpha}(\mathbf{x} - \xi, t - t') \sigma_{\alpha\beta}^P(\xi, t'); n=1,2,3; \alpha=1,2; \mathbf{x}, \xi \in \mathbb{R}^3$$

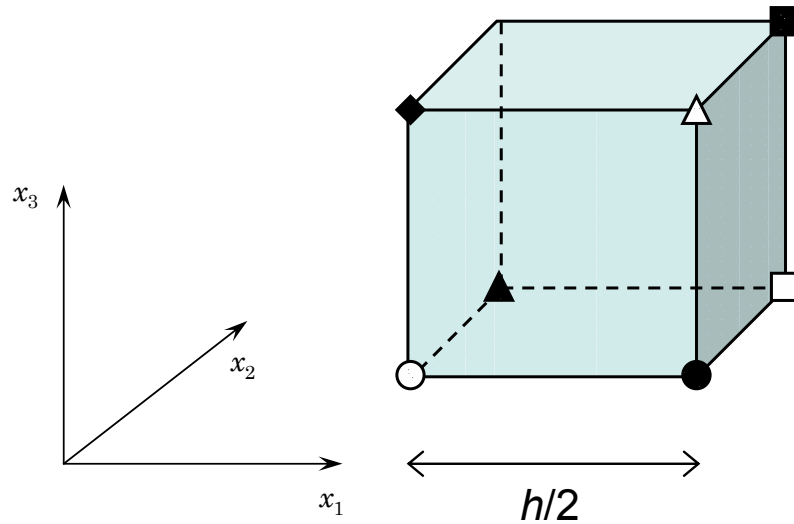
First neighbours decoupling (in the case of a 2 – D, pure in – plane rupture):



2. DISCRETIZATION OF EQUATIONS (FE, FD APPROACHES)

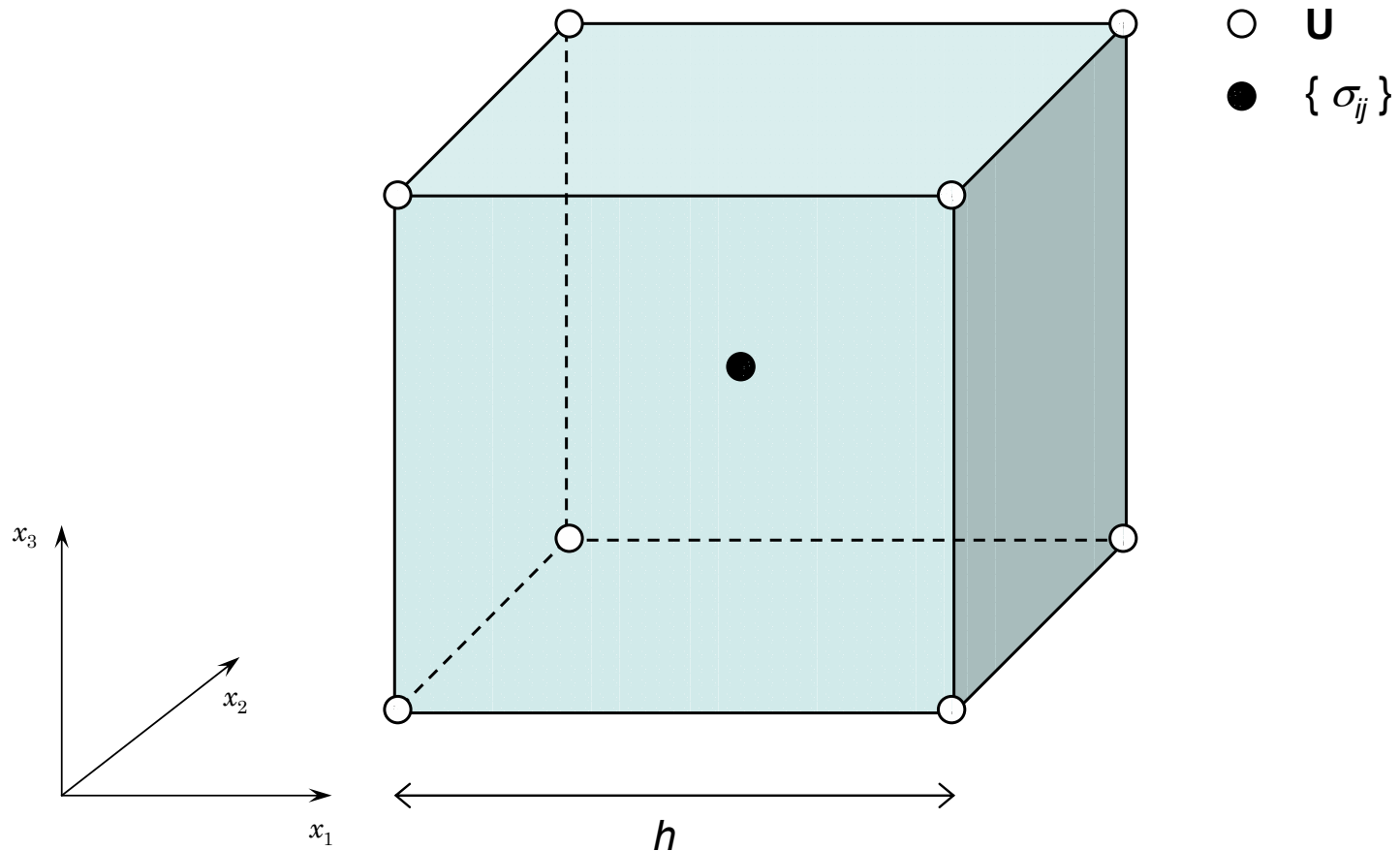
- Choice of the grid type

• **Staggered – grid (SG):**

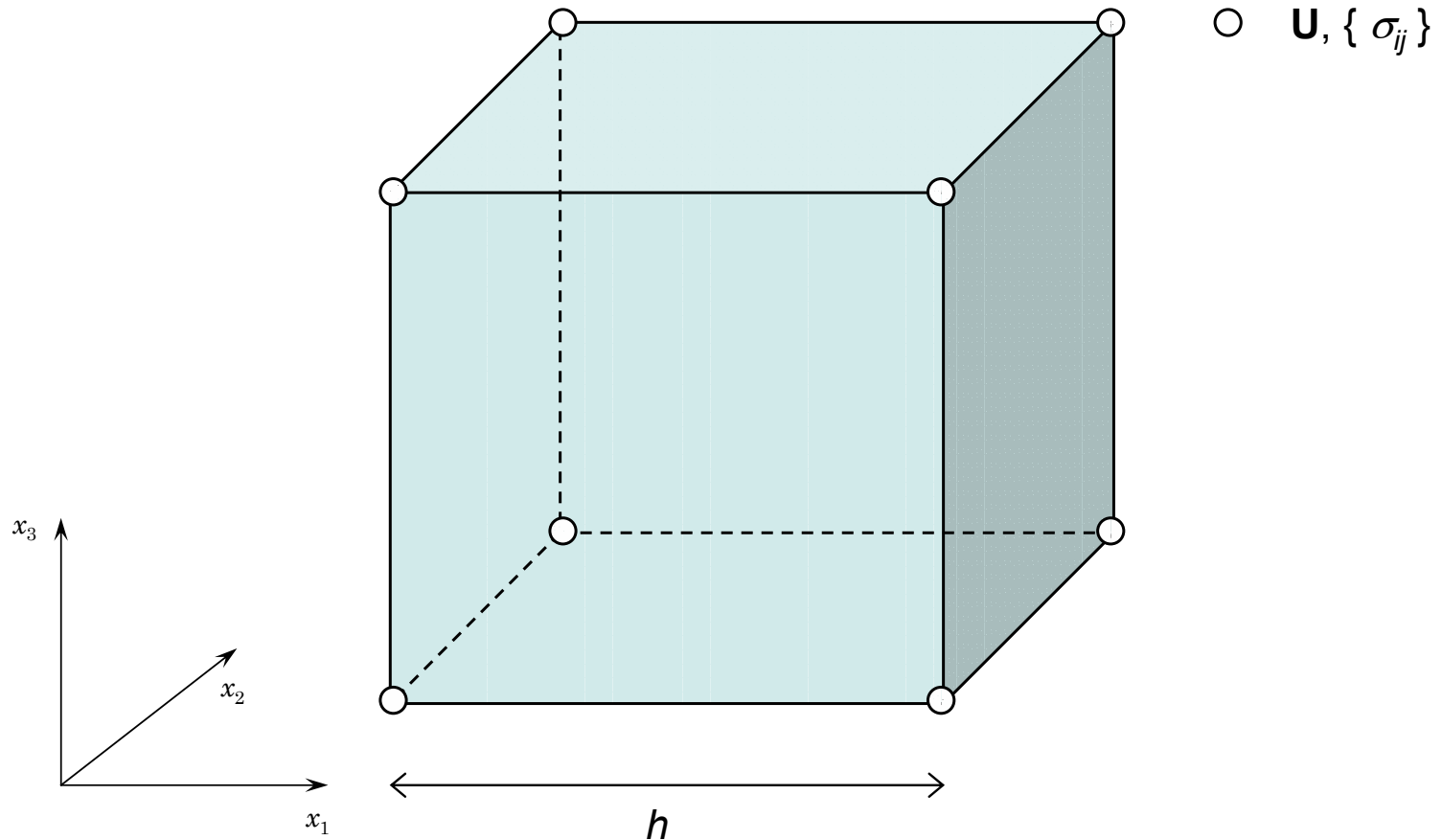


- U_1
- U_2
- △ U_3
- $\sigma_{11}, \sigma_{22}, \sigma_{33}$
- ▲ σ_{12}
- ◆ σ_{31}
- σ_{32}

- Partly Staggered – grid (PSG):



- **Conventional – grid (CG):**



Domain Boundaries Conditions

- * ***BOUNDARY:***
 - Bottom
 - Fixed
 - Absorbing
 - Top
 - Free surface
 - Topography
 - Coasts
 - Lateral
 - Cyclic
 - Absorbing

- Let us consider a boundary on i – direction. Indices i, j and k identify x_1, x_2 and x_3 axes, respectively. Apex m indicate the actual time level, while index l stands for component ($l = 1, 2, 3$).

- ***Fixed Boundary (FB):***

$$\begin{aligned}
 U_{1jk_l}^m &= 0, & \dot{U}_{1jk_l}^m &= 0 \\
 U_{i_{end}jk_l}^m &= 0, & \dot{U}_{i_{end}jk_l}^m &= 0
 \end{aligned}$$

- **Absorbing Boundary (AB):**

Left boundary:

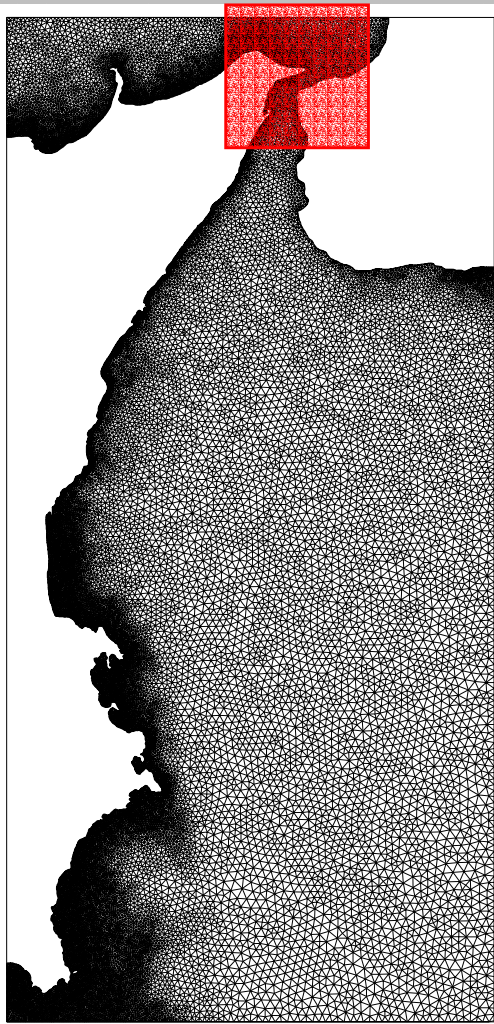
$$\begin{aligned}
 \dot{U}_{1jk_l}^m &= A_{01}\dot{U}_{2jk_l}^m + A_{02}\dot{U}_{3jk_l}^m \\
 &+ A_{10}\dot{U}_{1jk_l}^{m-1} + A_{11}\dot{U}_{2jk_l}^{m-1} + A_{12}\dot{U}_{3jk_l}^{m-1} \\
 &+ A_{20}\dot{U}_{1jk_l}^{m-2} + A_{21}\dot{U}_{2jk_l}^{m-2} + A_{22}\dot{U}_{3jk_l}^{m-2}
 \end{aligned}$$

Right boundary:

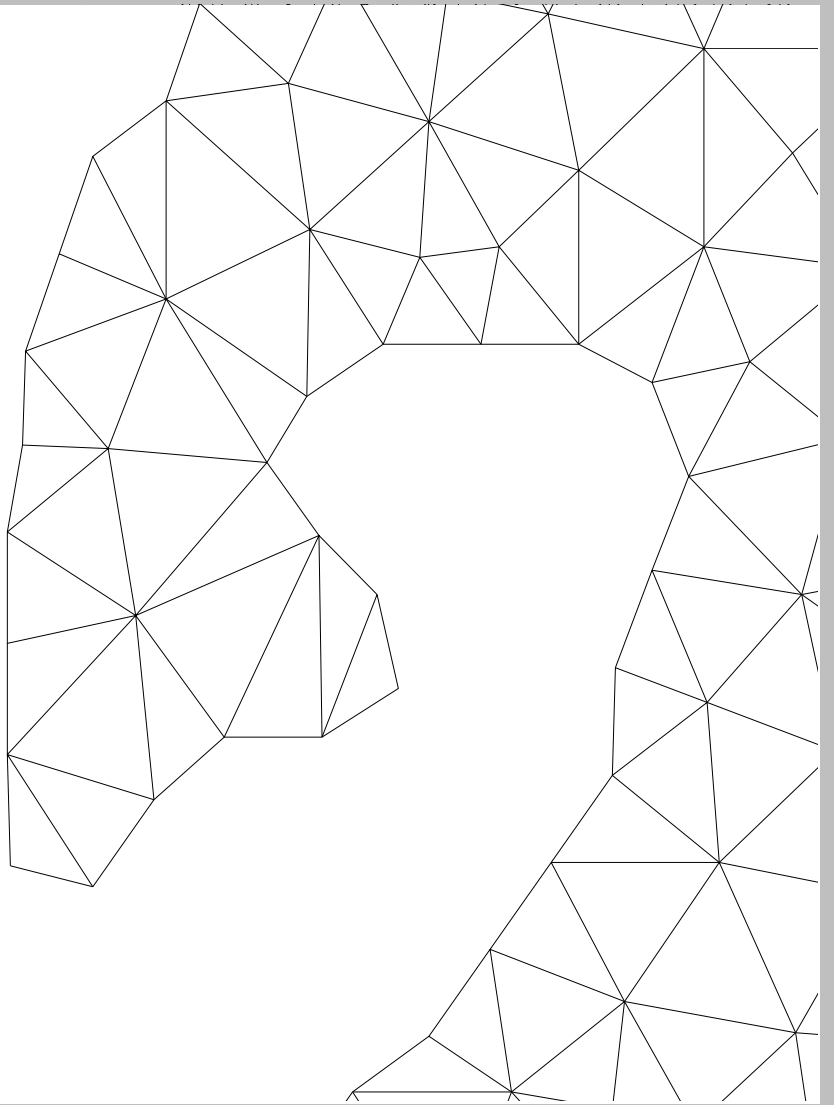
$$\begin{aligned}
 \dot{U}_{i_{end}jk_l}^m &= A_{01}\dot{U}_{i_{end}-1jk_l}^m + A_{02}\dot{U}_{i_{end}-2jk_l}^m \\
 &+ A_{10}\dot{U}_{i_{end}jk_l}^{m-1} + A_{11}\dot{U}_{i_{end}-1jk_l}^{m-1} + A_{12}\dot{U}_{i_{end}-2jk_l}^{m-1} \\
 &+ A_{20}\dot{U}_{i_{end}jk_l}^{m-2} + A_{21}\dot{U}_{i_{end}-1jk_l}^{m-2} + A_{22}\dot{U}_{i_{end}-2jk_l}^{m-2}
 \end{aligned}$$

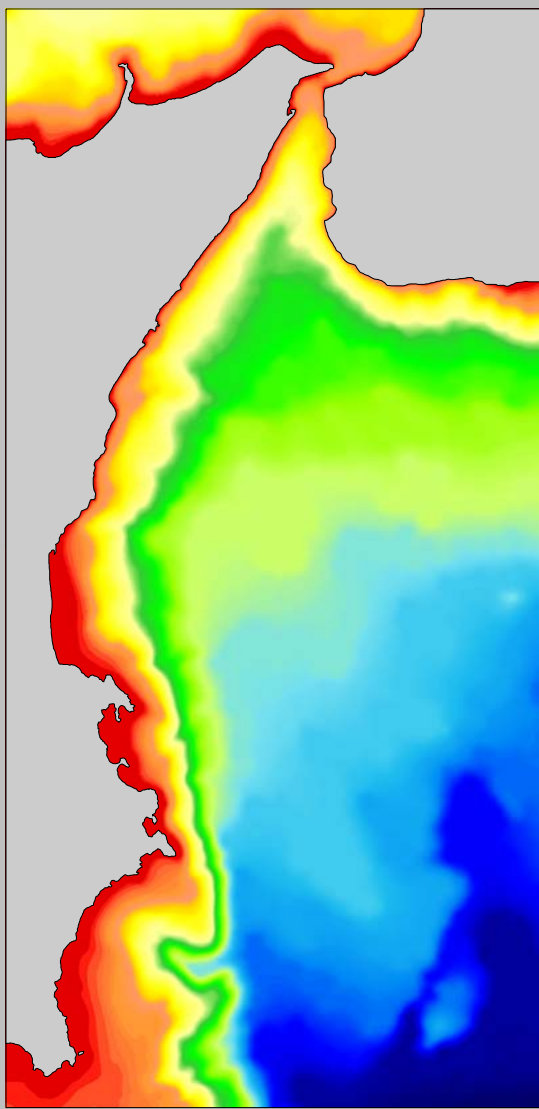
In the previous compact representation of ABCs (that follows *Moczo, 1998*):

- the coefficients $\{A_{pq}\}_{p,q=1,2,3}$ depend on the choice of ABC scheme (e. g. *Clayton and Engquist, 1977; Reynolds, 1978; Emerman and Stephen, 1983; Higdon, 1991; Peng and Toksöz, 1994, 1995; Liu and Archuleta, 2000, ...*);
- displacement components at actual time level m are derived by numerical integration from particle velocity components, after update;
- values in edges and in corners are derived from algebraic averaging of values of quantities belonging to walls;
- as it is a special boundary condition, there is no need to consider any rheology in the updated point.

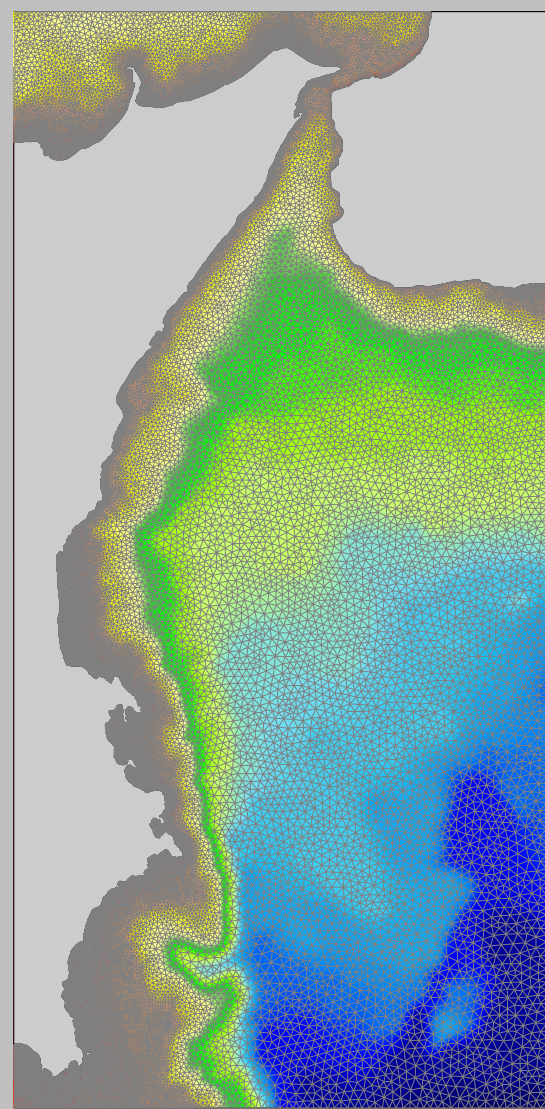
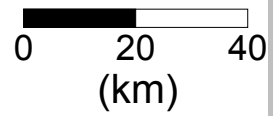
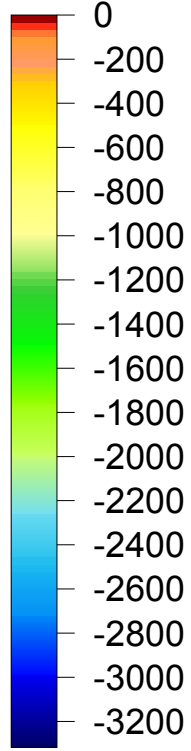


0 20 40 km





(m)








Number of nodes	30264
Number of elements	57733
Type of building block	Triangle
Minimum node distance	200 m
Maximum node distance	2000 m
References	Armigliato A., Tinti S., (2005), <i>EGU General Assebly</i> ; Tinti S., Armigliato A., Bortolucci E. (2001), <i>J. Seismol.</i> , 5 , 41-61.

Fault Boundary Conditions



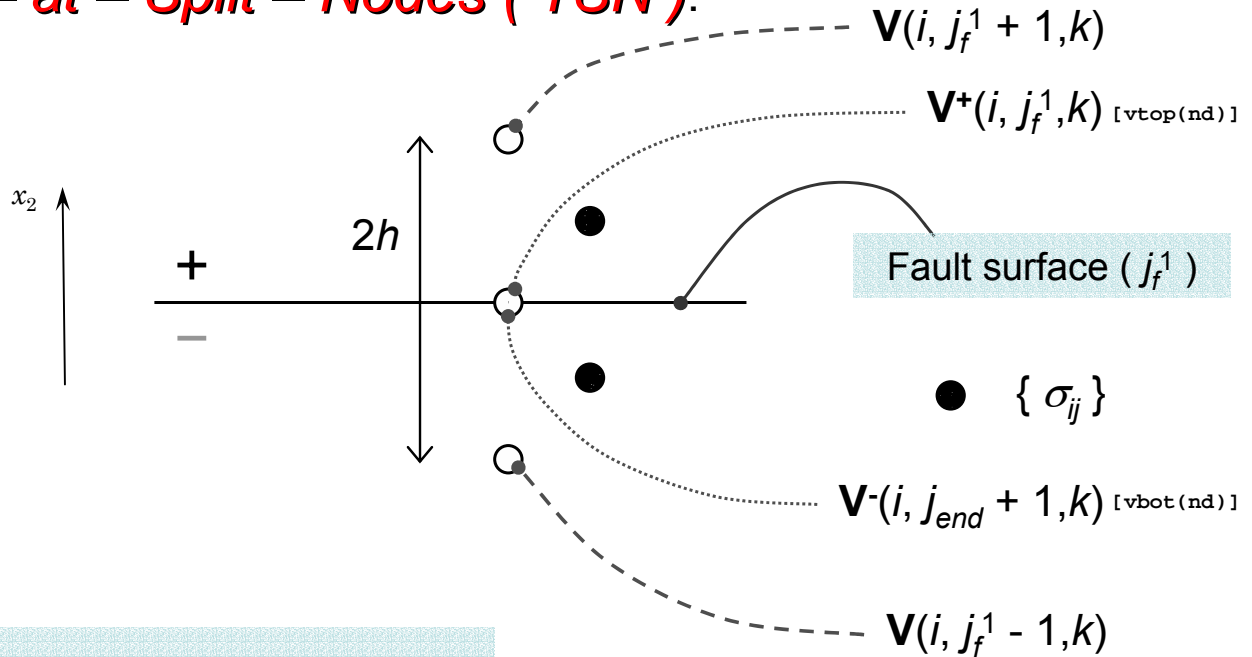
1. TYPE

- Traction – at – Split – Nodes (**TSN**): in 2 – D by *Andrews (1973)*; in 3 – D by *Day (1977)*, *Archuleta and Day (1980)*, *Day (1982a, 1982b)*, *Andrews (1999)*, *Bizzarri (2003)*, *Bizzarri and Cocco (2005)*, *Day et al. (2005)* 
- Stress – Glut (**SG**): *Backus and Mulchay (1976)*, *Andrews (1976)*
- Thin – zone (**TnZ**): *Virieux and Madariaga (1982)* 
- Thick – zone (**TkZ**): *Madariaga et al. (1998)* 

2. CONSTITUTIVE LAW

- Accounts for fault rheology
- and different physical phenomena occurring during the rupture process

- Traction – at – Split – Nodes (TSN):**

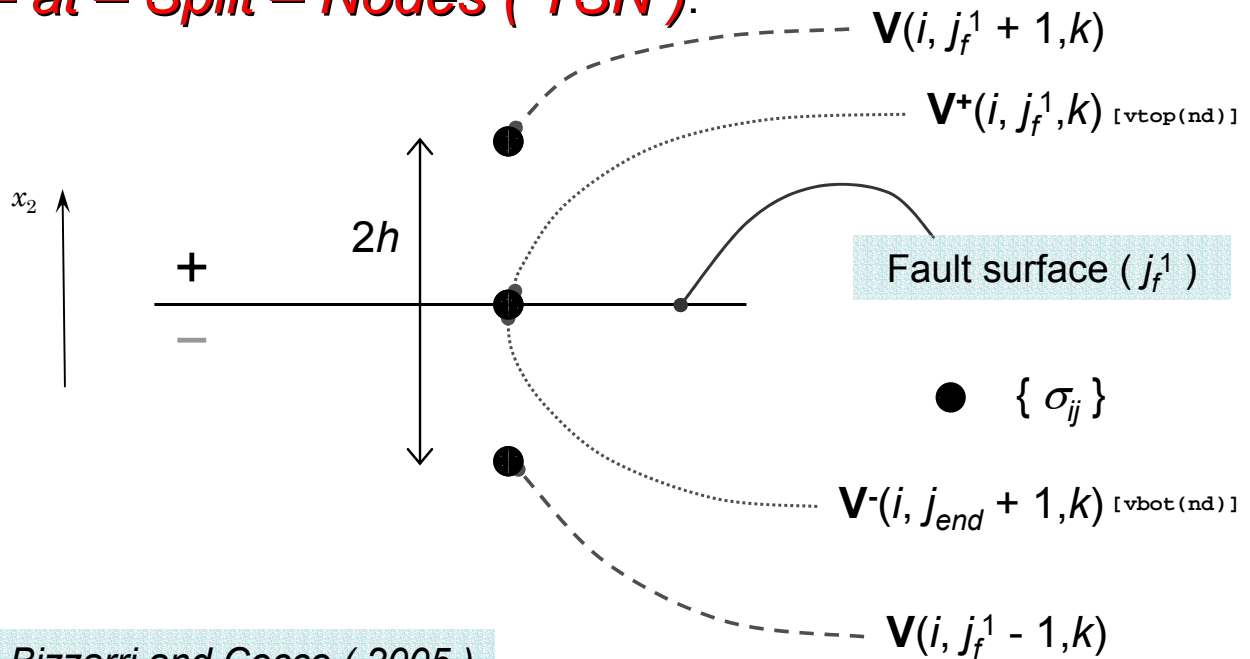


Day (1982b)

$$\Delta \mathbf{V} = \mathbf{V}^+ - \mathbf{V}^-$$

relative motion of the “ + ” side with respect to the “ - ” side. This value is used to calculate fault slip velocity \mathbf{v} , using the constitutive law

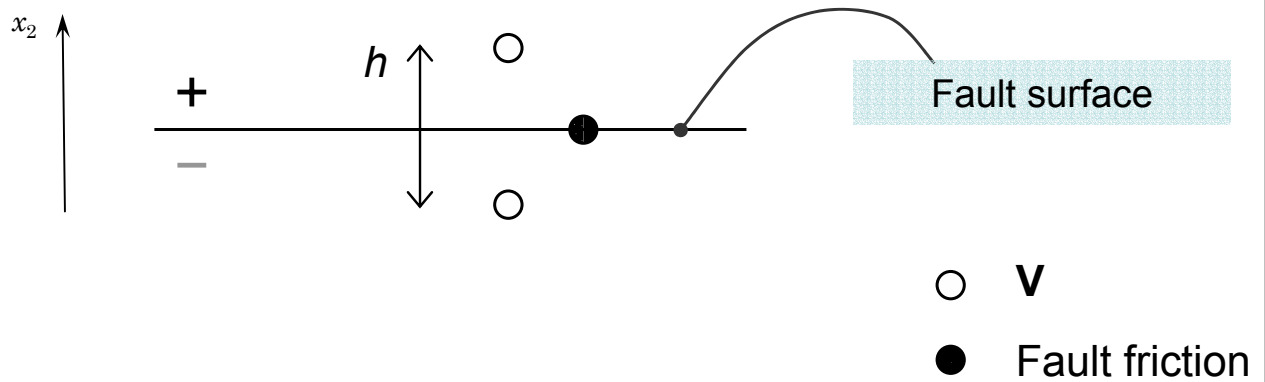
- **Traction – at – Split – Nodes (TSN):**



Andrews (1999), Bizzarri and Cocco (2005)

* **Discontinuum medium** (continuum mechanics equations of motion are applied to each half - space individually; the fault is an explicit discontinuity in displacement)

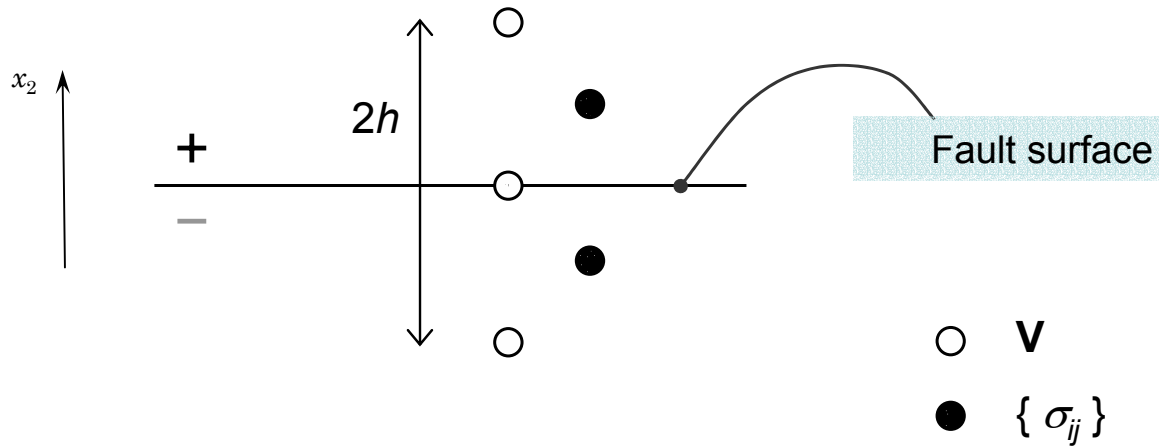
- **Thin – zone (TnZ):**



$\mathbf{v} = \mathbf{V}^+ - \mathbf{V}^-$ relative motion of the “+” side with respect to the “-” side.
It is calculated **over h**

* Continuum medium

- **Thick – zone (TkZ):**



$\mathbf{v} = \mathbf{V}^+ - \mathbf{V}^-$ relative motion of the “+” side with respect to the “-” side.
It is calculated **over $2h$**

* Continuum medium

Auxiliary Conditions



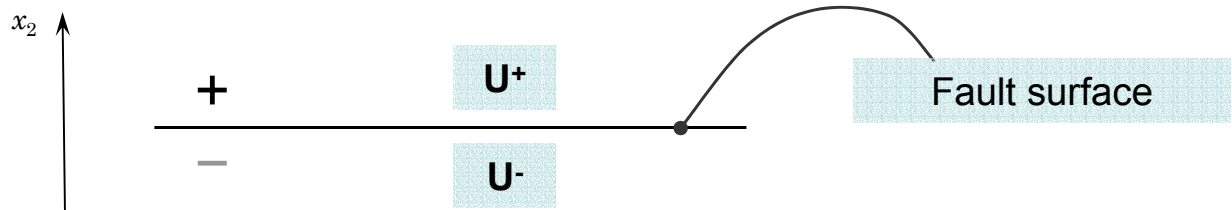
- * ***COLLINEARITY BETWEEN FAULT SHEAR TRACTION AND FAULT SLIP VELOCITY:***

$$\mathbf{T} \parallel \mathbf{v}$$

$$\text{(i. e. } \hat{\mathbf{T}} = \frac{\mathbf{v}}{\|\mathbf{v}\|} \text{)}.$$

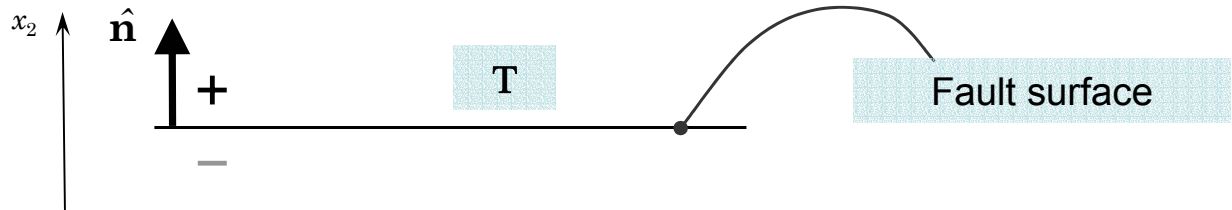
* **COLLINEARITY VS. ANTIPARALLELISM**

1. Definition of the fault slip u (i. e. displacement discontinuity):



$$u = U^+ - U^- \quad \text{relative motion of the “+” side with respect to the “-” side}$$

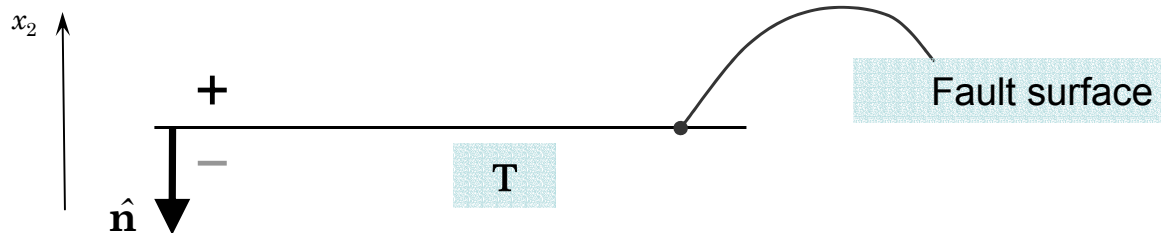
2. Fault surface orientation. Possibility A



T Shear traction that a particle located on the “+” side exercised on particle located in the “-” side

In this case the traction vector T is **collinear** to the direction of motion (namely to the fault slip vector u and therefore to the fault slip velocity vector v).

Possibility B



T Shear traction that a particle located on the “-” side exercised on particle located in the “+” side

In this case the traction vector T is **antiparallel** to the direction of motion (namely to the fault slip vector u and therefore to the fault slip velocity vector v).